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## Standard Test Methods for Tension Testing of Metallic Materials<sup>1</sup>

This standard is issued under the fixed designation E 8; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reappraisal. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reappraisal.

This standard has been approved for use by agencies of the Department of Defense to replace method 211.1 of Federal Test Method Standard No. 151b. Consult the DoD Index of Specifications and Standards for the specific year of issue which has been adopted by the Department of Defense.

### 1. Scope\*

1.1 These test methods cover the tension testing of metallic materials in any form at room temperature, specifically, the methods of determination of yield strength, yield point elongation, tensile strength, elongation, and reduction of area.

NOTE 1—A complete metric companion to Test Methods E 8 has been developed—E 8M; therefore, no metric equivalents are shown in these test methods.

NOTE 2—Gage lengths in these test methods are required to be 4D for most round specimens. Test specimens made from powder metallurgy (P/M) materials are exempt from this requirement by industry-wide agreement to keep the pressing of the material to a specific projected area and density.

NOTE 3—Exceptions to the provisions of these test methods may need to be made in individual specifications or test methods for a particular material. For examples, see Test Methods and Definitions A 370 and Methods B 557.

NOTE 4—Room temperature shall be considered to be 50 to 100°F unless otherwise specified.

1.2 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

### 2. Referenced Documents

#### 2.1 ASTM Standards:

- A 356/A 356M Specification for Heavy-Walled, Carbon, Low Alloy, and Stainless Steel Castings for Steam Turbines<sup>2</sup>
- A 370 Test Methods and Definitions for Mechanical Testing of Steel Products<sup>3</sup>
- B 557 Methods of Tension Testing Wrought and Cast Aluminum- and Magnesium-Alloy Products<sup>4</sup>
- E 4 Practices for Force Verification of Testing Machines<sup>5</sup>
- E 6 Terminology Relating to Methods of Mechanical Testing<sup>5</sup>

<sup>1</sup> These test methods are under the jurisdiction of ASTM Committee E-28 on Mechanical Testing and are the direct responsibility of Subcommittee E28.04 on Uniaxial Testing.

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<sup>2</sup> Annual Book of ASTM Standards, Vol 01.02.

<sup>3</sup> Annual Book of ASTM Standards, Vol 01.03.

<sup>4</sup> Annual Book of ASTM Standards, Vol 02.02.

<sup>5</sup> Annual Book of ASTM Standards, Vol 03.01.

- E 8M Test Methods for Tension Testing of Metallic Materials [Metric]<sup>5</sup>
- E 29 Practice for Using Significant Digits in Test Data to Determine Conformance with Specifications<sup>6</sup>
- E 83 Practice for Verification and Classification of Extensometers<sup>5</sup>
- E 345 Test Methods of Tension Testing of Metallic Foil<sup>5</sup>
- E 691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method<sup>6</sup>
- E 1012 Practice for Verification of Specimen Alignment Under Tensile Loading<sup>5</sup>

### 3. Terminology

3.1 *Definitions*—The definitions of terms relating to tension testing appearing in Terminology E 6 shall be considered as applying to the terms used in these test methods of tension testing. Additional terms being defined are as follows:

3.1.1 *discontinuous yielding*—a hesitation or fluctuation of force observed at the onset of plastic deformation, due to localized yielding. (The stress-strain curve need not appear to be discontinuous.)

3.1.2 *lower yield strength, LYS [FL<sup>-2</sup>]*—the minimum stress recorded during discontinuous yielding, ignoring transient effects.

3.1.3 *upper yield strength, UYS [FL<sup>-2</sup>]*—the first stress maximum (stress at first zero slope) associated with discontinuous yielding.

3.1.4 *yield point elongation, YPE*—the strain (expressed in percent) separating the stress-strain curve's first point of zero slope from the point of transition from discontinuous yielding to uniform strain hardening. If the transition occurs over a range of strain, the YPE end point is the intersection between (a) a horizontal line drawn tangent to the curve at the last zero slope and (b) a line drawn tangent to the strain hardening portion of the stress-strain curve at the point of inflection. If there is no point at or near the onset of yielding at which the slope reaches zero, the material has 0 % YPE.

### 4. Significance and Use

4.1 Tension tests provide information on the strength and ductility of materials under uniaxial tensile stresses. This information may be useful in comparisons of materials, alloy development, quality control, and design under certain circumstances.

<sup>6</sup> Annual Book of ASTM Standards, Vol 14.02.

\* A Summary of Changes section appears at the end of these test methods.

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4.2 The results of tension tests of specimens machined to standardized dimensions from selected portions of a part or material may not totally represent the strength and ductility properties of the entire end product or its in-service behavior in different environments.

4.3 These test methods are considered satisfactory for acceptance testing of commercial shipments. The test methods have been used extensively in the trade for this purpose.

## 5. Apparatus

5.1 *Testing Machines*—Machines used for tension testing shall conform to the requirements of Practices E 4. The forces used in determining tensile strength and yield strength shall be within the verified force application range of the testing machine as defined in Practices E 4.

### 5.2 Gripping Devices:

5.2.1 *General*—Various types of gripping devices may be used to transmit the measured force applied by the testing machine to the test specimens. To ensure axial tensile stress within the gage length, the axis of the test specimen should coincide with the center line of the heads of the testing machine. Any departure from this requirement may introduce bending stresses that are not included in the usual stress computation (force divided by cross-sectional area).

NOTE 5—The effect of this eccentric force application may be illustrated by calculating the bending moment and stress thus added. For a standard 1/2-in. diameter specimen, the stress increase is 1.5 percentage points for each 0.001 in. of eccentricity. This error increases to 2.24 percentage points/0.001 in. for a 0.350-in. diameter specimen and to 3.17 percentage points/0.001 in. for a 0.250-in. diameter specimen.

NOTE 6—Alignment methods are given in Practice E 1012.

5.2.2 *Wedge Grips*—Testing machines usually are equipped with wedge grips. These wedge grips generally furnish a satisfactory means of gripping long specimens of ductile metal and flat plate test specimens such as those shown in Fig. 1. If, however, for any reason, one grip of a pair advances farther than the other as the grips tighten, an undesirable bending stress may be introduced. When liners are used behind the wedges, they must be of the same thickness and their faces must be flat and parallel. For best results, the wedges should be supported over their entire lengths by the heads of the testing machine. This requires that liners of several thicknesses be available to cover the range of specimen thickness. For proper gripping, it is desirable that the entire length of the serrated face of each wedge be in contact with the specimen. Proper alignment of wedge grips and liners is illustrated in Fig. 2. For short specimens and for specimens of many materials it is generally necessary to use machined test specimens and to use a special means of gripping to ensure that the specimens, when under load, shall be as nearly as possible in uniformly distributed pure axial tension (see 5.2.3, 5.2.4, and 5.2.5).

5.2.3 *Grips for Threaded and Shouldered Specimens and Brittle Materials*—A schematic diagram of a gripping device for threaded-end specimens is shown in Fig. 3, while Fig. 4 shows a device for gripping specimens with shouldered ends. Both of these gripping devices should be attached to the heads of the testing machine through properly lubricated spherical-seated bearings. The distance between spherical bearings should be as great as feasible.

5.2.4 *Grips for Sheet Materials*—The self-adjusting grips

shown in Fig. 5 have proven satisfactory for testing sheet materials that cannot be tested satisfactorily in the usual type of wedge grips.

5.2.5 *Grips for Wire*—Grips of either the wedge or snubbing types as shown in Figs. 5 and 6 or flat wedge grips may be used.

5.3 *Dimension-Measuring Devices*—Micrometers and other devices used for measuring linear dimensions shall be accurate and precise to at least one half the smallest unit to which the individual dimension is required to be measured.

## 6. Test Specimens

### 6.1 General:

6.1.1 Test specimens shall be either substantially full size or machined, as prescribed in the product specifications for the material being tested.

6.1.2 Improperly prepared test specimens often are the reason for unsatisfactory and incorrect test results. It is important, therefore, that care be exercised in the preparation of specimens, particularly in the machining, to ensure the desired precision and bias in test results.

6.1.3 It is desirable to have the cross-sectional area of the specimen smallest at the center of the reduced section to ensure fracture within the gage length. For this reason, a small taper is permitted in the reduced section of each of the specimens described in the following sections.

6.1.4 For brittle materials it is desirable to have fillets of large radius at the ends of the gage length.

6.2 *Plate-Type Specimens*—The standard plate-type test specimen is shown in Fig. 1. This specimen is used for testing metallic materials in the form of plate, shapes, and flat material having a nominal thickness of 3/16 in. or over. When product specifications so permit, other types of specimens may be used, as provided in 6.3, 6.4, and 6.5.

### 6.3 Sheet-Type Specimens:

6.3.1 The standard sheet-type test specimen is shown in Fig. 1. This specimen is used for testing metallic materials in the form of sheet, plate, flat wire, strip, band, hoop, rectangles, and shapes ranging in nominal thickness from 0.005 to 3/4 in. When product specifications so permit, other types of specimens may be used, as provided in 6.2, 6.4, and 6.5.

NOTE 7—Test Methods E 345 may be used for tension testing of materials in thicknesses up to 0.0059 in.

6.3.2 Pin ends as shown in Fig. 7 may be used. In order to avoid buckling in tests of thin and high-strength materials, it may be necessary to use stiffening plates at the grip ends.

### 6.4 Round Specimens:

6.4.1 The standard 0.500-in. diameter round test specimen shown in Fig. 8 is used quite generally for testing metallic materials, both cast and wrought.

6.4.2 Figure 8 also shows small-size specimens proportional to the standard specimen. These may be used when it is necessary to test material from which the standard specimen or specimens shown in Fig. 1 cannot be prepared. Other sizes of small round specimens may be used. In any such small-size specimen it is important that the gage length for measurement of elongation be four times the diameter of the specimen.

6.4.3 The shape of the ends of the specimen outside of the gage length shall be suitable to the material and of a shape to fit the holders or grips of the testing machine so that the



forces may be applied axially. Figure 9 shows specimens with various types of ends that have given satisfactory results.

6.5 *Specimens for Sheet, Strip, Flat Wire, and Plate*—In testing sheet, plate, flat wire, and strip one of the following types of specimens shall be used:

6.5.1 For material ranging in nominal thickness from 0.005 to 3/4 in., use the sheet-type specimen described in 6.3.

NOTE 8—Attention is called to the fact that either of the flat specimens described in 6.2 and 6.3 may be used for material from 3/16 to 3/4 in. in thickness, and one of the round specimens described in 6.4 may also be used for material 1/2 in. or more in thickness.

6.5.2 For material having a nominal thickness of 3/16 in. or over (Note 8), use the plate-type specimen described in 6.2.

6.5.3 For material having a nominal thickness of 1/2 in. or over (Note 8), use the largest practical size of specimen described in 6.4.

6.6 *Specimens for Wire, Rod, and Bar*:

6.6.1 For round wire, rod, and bar, test specimens having the full cross-sectional area of the wire, rod, or bar shall be used wherever practicable. The gage length for the measurement of elongation of wire less than 1/8 in. in diameter shall be as prescribed in product specifications. In testing wire, rod, or bar that has a 1/8-in. or larger diameter, unless otherwise specified, a gage length equal to four times the diameter shall be used. The total length of the specimens shall be at least equal to the gage length plus the length of material required for the full use of the grips employed.

6.6.2 For wire of octagonal, hexagonal, or square cross section, for rod or bar of round cross section where the specimen required in 6.6.1 is not practicable, and for rod or bar of octagonal, hexagonal, or square cross section, one of the following types of specimens shall be used:

6.6.2.1 *Full Cross Section* (Note 9)—It is permissible to reduce the test section slightly with abrasive cloth or paper, or machine it sufficiently to ensure fracture within the gage marks. For material not exceeding 0.188 in. in diameter or distance between flats, the cross-sectional area may be reduced to not less than 90 % of the original area without changing the shape of the cross section. For material over 0.188 in. in diameter or distance between flats, the diameter or distance between flats may be reduced by not more than 0.010 in. without changing the shape of the cross section. Square, hexagonal, or octagonal wire or rod not exceeding 0.188 in. between flats may be turned to a round having a cross-sectional area not smaller than 90 % of the area of the maximum inscribed circle. Fillets, preferably with a radius of 3/8 in., but not less than 1/8 in., shall be used at the ends of the reduced sections. Square, hexagonal, or octagonal rod over 0.188 in. between flats may be turned to a round having a diameter no smaller than 0.010 in. less than the original distance between flats.

NOTE 9—The ends of copper or copper alloy specimens may be flattened 10 to 50 % from the original dimension in a jig similar to that shown in Fig. 10, to facilitate fracture within the gage marks. In flattening the opposite ends of the test specimen, care shall be taken to ensure that the four flattened surfaces are parallel and that the two parallel surfaces on the same side of the axis of the test specimen lie in the same plane.

6.6.2.2 For rod and bar, the largest practical size of round specimen as described in 6.4 may be used in place of a test specimen of full cross section. Unless otherwise specified in

the product specification, specimens shall be parallel to the direction of rolling or extrusion.

6.7 *Specimens for Rectangular Bar*—In testing rectangular bar one of the following types of specimens shall be used:

6.7.1 *Full Cross Section*—It is permissible to reduce the width of the specimen throughout the test section with abrasive cloth or paper, or by machining sufficiently to facilitate fracture within the gage marks, but in no case shall the reduced width be less than 90 % of the original. The edges of the midlength of the reduced section not less than 3/4 in. in length shall be parallel to each other and to the longitudinal axis of the specimen within 0.002 in. Fillets, preferably with a radius of 3/8 in. but not less than 1/8 in. shall be used at the ends of the reduced sections.

6.7.2 Rectangular bar of thickness small enough to fit the grips of the testing machine but of too great width may be reduced in width by cutting to fit the grips, after which the cut surfaces shall be machined or cut and smoothed to ensure failure within the desired section. The reduced width shall be not less than the original bar thickness. Also, one of the types of specimens described in 6.2, 6.3, and 6.4 may be used.

6.8 *Shapes, Structural and Other*—In testing shapes other than those covered by the preceding sections, one of the types of specimens described in 6.2, 6.3, and 6.4 shall be used.

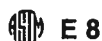
6.9 *Specimens for Pipe and Tube* (Note 10):

6.9.1 For all small tube (Note 10), particularly sizes 1 in. and under in nominal outside diameter, and frequently for larger sizes, except as limited by the testing equipment, it is standard practice to use tension test specimens of full-size tubular sections. Snug-fitting metal plugs shall be inserted far enough into the ends of such tubular specimens to permit the testing machine jaws to grip the specimens properly. The plugs shall not extend into that part of the specimen on which the elongation is measured. Elongation is measured over a length of 4D unless otherwise stated in the product specification. Figure 11 shows a suitable form of plug, the location of the plugs in the specimen, and the location of the specimen in the grips of the testing machine.

NOTE 10—The term "tube" is used to indicate tubular products in general, and includes pipe, tube, and tubing.

6.9.2 For large-diameter tube that cannot be tested in full section, longitudinal tension test specimens shall be cut as indicated in Fig. 12. Specimens from welded tube shall be located approximately 90° from the weld. If the tube-wall thickness is under 3/4 in., either a specimen of the form and dimensions shown in Fig. 13 or one of the small-size specimens proportional to the standard 1/2-in. specimen, as mentioned in 6.4.2 and shown in Fig. 8, shall be used. Specimens of the type shown in Fig. 13 may be tested with grips having a surface contour corresponding to the curvature of the tube. When grips with curved faces are not available, the ends of the specimens may be flattened without heating. If the tube-wall thickness is 3/4 in. or over, the standard specimen shown in Fig. 8 shall be used.

NOTE 11—In clamping of specimens from pipe and tube (as may be done during machining) or in flattening specimen ends (for gripping), care must be taken so as not to subject the reduced section to any deformation or cold work, as this would alter the mechanical properties.



**TABLE 1 Details of Test Coupon Design for Castings (See Fig. 16)**

**NOTE 1—Test Coupons for Large and Heavy Steel Castings:** The test coupons in Fig. 16 are to be used for large and heavy steel castings. However, at the option of the foundry the cross-sectional area and length of the standard coupon may be increased as desired. This provision does not apply to Specification A 356/A 356M.

**NOTE 2—Bend Bar:** If a bend bar is required, an alternate design (as shown by dotted lines in Fig. 16) is indicated.

	Log Design (5 in.)		Riser Design
1. <i>L</i> (length)	A 5-in. minimum length will be used. This length may be increased at the option of the foundry to accommodate additional test bars (see Note 1).	1. <i>L</i> (length)	The length of the riser at the base will be the same as the top length of the leg. The length of the riser at the top therefore depends on the amount of taper added to the riser.
2. End taper	Use of and size of end taper is at the option of the foundry.	2. Width	The width of the riser at the base of a multiple-leg coupon shall be $n(2\frac{1}{4} \text{ in.}) - \frac{1}{8} \text{ in.}$ where $n$ equals the number of legs attached to the coupon. The width of the riser at the top is therefore dependent on the amount of taper added to the riser.
3. Height	1 $\frac{1}{4}$ in.		
4. Width (at top)	1 $\frac{1}{4}$ in. (see Note 1)		
5. Radius (at bottom)	$\frac{1}{2}$ in. max		
6. Spacing between legs	A $\frac{1}{2}$ -in. radius will be used between the legs.		
7. Location of test bars	The tensile, bend, and impact bars will be taken from the lower portion of the leg (see Note 2).		
8. Number of legs	The number of legs attached to the coupon is at the option of the foundry providing they are equispaced according to item 6.	3. <i>T</i> (riser taper) Height	Use of and size is at the option of the foundry. The minimum height of the riser shall be 2 in. The maximum height is at the option of the foundry for the following reasons: (a) many risers are cast open, (b) different compositions may require variation in risering for soundness, or (c) different pouring temperatures may require variation in risering for soundness.
9. <i>R<sub>s</sub></i>	Radius from 0 to approximately $\frac{1}{16}$ in.		

6.9.3 Transverse tension test specimens for tube may be taken from rings cut from the ends of the tube as shown in Fig. 14. Flattening of the specimen may be either after separating as in *A*, or before separating as in *B*. Transverse tension test specimens for large tube under  $\frac{3}{4}$  in. in wall thickness shall be either of the small-size specimens shown in Fig. 8 or of the form and dimensions shown for Specimen 2 in Fig. 13. When using the latter specimen, either or both surfaces of the specimen may be machined to secure a uniform thickness, provided not more than 15 % of the normal wall thickness is removed from each surface. For large tube  $\frac{3}{4}$  in. and over in wall thickness, the standard specimen shown in Fig. 8 shall be used for transverse tension tests. Specimens for transverse tension tests on large welded tube to determine the strength of welds shall be located perpendicular to the welded seams, with the welds at about the middle of their lengths.

6.10 *Specimens for Forgings*—For testing forgings, the largest round specimen described in 6.4 shall be used. If round specimens are not feasible, then the largest specimen described in 6.5 shall be used.

6.11 *Specimens for Castings*—In testing castings either the standard specimen shown in Fig. 8 or the specimen shown in Fig. 15 shall be used unless otherwise provided in the product specifications.

6.11.1 Test coupons for castings shall be made as shown in Fig. 16 and Table 1.

6.12 *Specimen for Malleable Iron*—For testing malleable iron the test specimen shown in Fig. 17 shall be used, unless otherwise provided in the product specifications.

6.13 *Specimen for Die Castings*—For testing die castings the test specimen shown in Fig. 18 shall be used unless otherwise provided in the product specifications.

6.14 *Specimens for Powder Metallurgy (P/M) Materials*—For testing powder metallurgy (P/M) materials the test specimens shown in Figs. 19 and 20 shall be used, unless

otherwise provided in the product specifications. When making test specimens in accordance with Fig. 19, shallow transverse grooves, or ridges, may be pressed in the ends to allow gripping by jaws machined to fit the grooves or ridges. Because of shape and other factors, the flat unmachined tensile test specimen (Fig. 19) in the heat treated condition will have an ultimate tensile strength of 50 % to 85 % of that determined in a machined round tensile test specimen (Fig. 20) of like composition and processing.

#### 6.15 Gage Length of Test Specimens:

6.15.1 The gage length for the determination of elongation shall be in accordance with the product specifications for the material being tested. Gage marks shall be stamped lightly with a punch, scribed lightly with dividers or drawn with ink as preferred. For material that is sensitive to the effect of slight notches and for small specimens, the use of layout ink will aid in locating the original gage marks after fracture.

6.15.2 Extensometers with gage lengths equal to or shorter than the nominal gage length (dimension shown as “G-Gage Length” in the accompanying figures) of the specimen may be used to determine the yield phenomenon.

#### 6.16 Location of Test Specimens:

6.16.1 Unless otherwise specified, the axis of the test specimen shall be located as follows:

6.16.1.1 At the center for products 1 $\frac{1}{2}$  in. or less in thickness, diameter, or distance between flats.

6.16.1.2 Midway from the center to the surface for products over 1 $\frac{1}{2}$  in. in thickness, diameter, or distance between flats.

6.16.2 For forgings, specimens shall be taken as provided in the applicable product specifications, either from the predominant or thickest part of the forging from which a coupon can be obtained, or from a prolongation of the forging, or from separately forged coupons representative of the forging. When not otherwise specified, the axis of the





specimen shall be parallel to the direction of grain flow.

6.17 *Surface Finish of Specimens*—When materials are tested with surface conditions other than as manufactured, the surface finish of the test specimens shall be as provided in the applicable product specifications.

NOTE 12—Particular attention should be given to the uniformity and quality of surface finishes of specimens for high strength and very low ductility materials since this has been shown to be a factor in the variability of test results.

7. Procedures

7.1 *Measurement of Dimensions of Test Specimens:*

7.1.1 To determine the cross-sectional area of a test specimen, measure the dimensions of the cross section at the center of the reduced section. For referee testing of specimens under 3/16 in. in their least dimension, measure the dimensions where the least cross-sectional area is found. Measure and record the cross-sectional dimensions of tension test specimens 0.200 in. and over to the nearest 0.001 in.; the cross-sectional dimensions from 0.100 in. but less than 0.200 in., to the nearest 0.0005 in.; the cross-sectional dimensions from 0.020 in. but less than 0.100 in., to the nearest 0.0001 in.; and when practical, the cross-sectional dimensions less than 0.020 in., to at least the nearest 1 % but in all cases to at least the nearest 0.0001 in.

NOTE 13—Accurate and precise measurement of specimen dimensions can be one of the most critical aspects of tension testing, depending on specimen geometry. See Appendix X2 for additional information.

NOTE 14—Rough surfaces due to the manufacturing process such as hot rolling, metallic coating, etc., may lead to inaccuracy of the computed areas greater than the measured dimensions would indicate. Therefore, cross-sectional dimensions of test specimens with rough surfaces due to processing may be measured and recorded to the nearest 0.001 in.

7.1.2 Determine cross-sectional areas of full-size test specimens of nonsymmetrical cross sections by weighing a length not less than 20 times the largest cross-sectional dimension and using the value of density of the material. Determine the weight to the nearest 0.5 % or less.

7.1.3 When using specimens of the type shown in Fig. 13 taken from tubes, the cross-sectional area shall be determined as follows:

If  $D/W \leq 6$ :

$$A = [(W/4) \times (D^2 - W^2)^{1/2}] + [(D^2/4) \times \arcsin(W/D)] - [(W/4) \times ((D - 2T)^2 - W^2)^{1/2}] - [((D - 2T)/2)^2 \times \arcsin(W/(D - 2T))]$$

where:

- A = exact cross-sectional area, in.<sup>2</sup>,
- W = width of the specimen in the reduced section, in.,
- D = measured outside diameter of the tube, in., and
- T = measured wall thickness of the specimen, in.

arcsin values to be in radians

If  $D/W > 6$ , the exact equation or the following equation may be used:

$$A = W \times T$$

where:

- A = approximate cross-sectional area, in.<sup>2</sup>,
- W = width of the specimen in the reduced section, in., and
- T = measured wall thickness of the specimen, in.

NOTE 15—See X2.8 for cautionary information on measurements and calculations for specimens taken from large-diameter tubing.

7.2 *Zeroing of the Testing Machine:*

7.2.1 The testing machine shall be set up in such a manner that zero force indication signifies a state of zero force on the specimen. Any force (or preload) imparted by the gripping of the specimen (see Note 16) must be indicated by the force measuring system unless the preload is physically removed prior to testing. Artificial methods of removing the preload on the specimen, such as taring it out by a zero adjust pot or removing it mathematically by software, are prohibited because these would affect the accuracy of the test results.

NOTE 16—Preloads generated by gripping of specimens may be either tensile or compressive in nature and may be the result of such things as:

- grip design
- malfunction of gripping apparatus (sticking, binding, etc.)
- excessive gripping force
- sensitivity of the control loop

NOTE 17—It is the operator's responsibility to verify that an observed preload is acceptable and to ensure that grips operate in a smooth manner. Unless otherwise specified, it is recommended that momentary (dynamic) forces due to gripping not exceed 20 % of the material's nominal yield strength and that static preloads not exceed 10 % of the material's nominal yield strength.

7.3 *Gripping of the Test Specimen:*

7.3.1 For specimens with reduced sections, gripping of the specimen shall be restricted to the grip section, because gripping in the reduced section or in the fillet can significantly affect test results.

7.4 *Speed of Testing:*

7.4.1 Speed of testing may be defined in terms of (a) rate of straining of the specimen, (b) rate of stressing of the specimen, (c) rate of separation of the two heads of the testing machine during a test, (d) the elapsed time for completing part or all of the test, or (e) free-running crosshead speed (rate of movement of the crosshead of the testing machine when not under load).

7.4.2 Specifying suitable numerical limits for speed and selection of the method are the responsibilities of the product committees. Suitable limits for speed of testing should be specified for materials for which the differences resulting from the use of different speeds are of such magnitude that the test results are unsatisfactory for determining the acceptability of the material. In such instances, depending upon the material and the use for which the test results are intended, one or more of the methods described in the following paragraphs is recommended for specifying speed of testing.

NOTE 18—Speed of testing can affect test values because of the rate sensitivity of materials and the temperature-time effects.

7.4.2.1 *Rate of Straining*—The allowable limits for rate of straining shall be specified in inches per inch per minute. Some testing machines are equipped with pacing or indicating devices for the measurement and control of rate of straining, but in the absence of such a device the average rate of straining can be determined with a timing device by observing the time required to effect a known increment of strain.

7.4.2.2 *Rate of Stressing*—The allowable limits for rate of stressing shall be specified in pounds per square inch per



minute. Many testing machines are equipped with pacing or indicating devices for the measurement and control of the rate of stressing, but in the absence of such a device the average rate of stressing can be determined with a timing device by observing the time required to apply a known increment of stress.

**7.4.2.3 Rate of Separation of Heads During Tests**—The allowable limits for rate of separation of the heads of the testing machine, during a test, shall be specified in inches per inch of length of reduced section (or distance between grips for specimens not having reduced sections) per minute. The limits for the rate of separation may be further qualified by specifying different limits for various types and sizes of specimens. Many testing machines are equipped with pacing or indicating devices for the measurement and control of the rate of separation of the heads of the machine during a test, but in the absence of such a device the average rate of separation of the heads can be experimentally determined by using suitable length-measuring and timing devices.

**7.4.2.4 Elapsed Time**—The allowable limits for the elapsed time from the beginning of force application (or from some specified stress) to the instant of fracture, to the maximum force, or to some other stated stress, shall be specified in minutes or seconds. The elapsed time can be determined with a timing device.

**7.4.2.5 Free-Running Crosshead Speed**—The allowable limits for the rate of movement of the crosshead of the testing machine, with no force applied by the testing machine, shall be specified in inches per inch of length of reduced section (or distance between grips for specimens not having reduced sections) per minute. The limits for the crosshead speed may be further qualified by specifying different limits for various types and sizes of specimens. The average crosshead speed can be experimentally determined by using suitable length-measuring and timing devices.

NOTE 19—For machines not having crossheads or having stationary crossheads, the phrase “free-running crosshead speed” may be interpreted to mean the free-running rate of grip separation.

**7.4.3 Speed of Testing When Determining Yield Properties**—Unless otherwise specified, any convenient speed of testing may be used up to one half the specified yield strength or up to one quarter the specified tensile strength, whichever is smaller. The speed above this point shall be within the limits specified. If different speed limitations are required for use in determining yield strength, yield point elongation, tensile strength, elongation, and reduction of area, they should be stated in the product specifications. In the absence of any specified limitations on speed of testing, the following general rules shall apply:

NOTE 20—In the previous and following paragraphs, the yield properties referred to include yield strength and yield point elongation.

**7.4.3.1** The speed of testing shall be such that the forces and strains used in obtaining the test results are accurately indicated.

**7.4.3.2** When performing a test to determine yield properties, the rate of stress application shall be between 10 000 and 100 000 psi/min.

NOTE 21—When a specimen being tested begins to yield, the stressing rate decreases and may even become negative in the case of a specimen with discontinuous yielding. To maintain a constant stressing rate would require the testing machine to operate at extremely high

speeds and, in many cases, this is not practical. The speed of the testing machine shall not be increased in order to maintain a stressing rate when the specimen begins to yield. In practice, it is simpler to use either a strain rate, a rate of separation of the heads, or a free-running crosshead speed which approximates the desired stressing rate. As an example, use a strain rate that is less than 100 000 psi divided by the nominal Young's Modulus of the material being tested. As another example, find a rate of separation of the heads through experimentation which would approximate the desired stressing rate prior to the onset of yielding, and maintain that rate of separation of the heads through the region that yield properties are determined. While both of these methods will provide similar rates of stressing and straining prior to the onset of yielding, the rates of stressing and straining may be different in the region where yield properties are determined. This difference is due to the change in the rate of elastic deformation of the testing machine, before and after the onset of yielding. In addition, the use of any of the methods other than rate of straining may result in different stressing and straining rates when using different testing machines, due to differences in the stiffness of the testing machines used.

**7.4.4 Speed of Testing When Determining Tensile Strength**—In the absence of any specified limitations on speed of testing, the following general rules shall apply. When determining only the tensile strength, or after the yield properties have been determined, the speed of the testing machine may be increased to correspond to a strain rate between 0.05 and 0.5 in./in./min. An extensometer and strain rate indicator may be used to set the strain rate. If an extensometer and strain rate indicator are not used to set this strain rate, the speed of the testing machine shall be set between 0.05 and 0.5 in./in. of the length of the reduced section (or distance between the grips for specimens not having reduced sections) per minute.

**7.5 Determination of Yield Strength**—Determine yield strength by any of the methods described in 7.5.1 to 7.5.5.

**7.5.1 Offset Method**—To determine the yield strength by the offset method, it is necessary to secure data (autographic or numerical) from which a stress-strain diagram may be drawn. Then on the stress-strain diagram (Fig. 21) lay off  $Om$  equal to the specified value of the offset, draw  $mn$  parallel to  $OA$ , and thus locate  $r$ , the intersection of  $mn$  with the stress-strain diagram (Note 27). In reporting values of yield strength obtained by this method, the specified value of offset used should be stated in parentheses after the term yield strength. Thus:

$$\text{Yield strength (offset = 0.2 \%)} = 52\,000 \text{ psi}$$

In using this method, a Class B2 or better extensometer (see Practice E 83) shall be used.

NOTE 22—There are two general types of extensometers, averaging and non-averaging, the use of which is dependent on the product tested. For most machined specimens, there are minimal differences. However, for some forgings and tube sections, significant differences in measured yield strength can occur. For these cases, it is recommended that the averaging type be used.

NOTE 23—When there is a disagreement over yield properties, the offset method for determining yield strength is recommended as the referee method.

**7.5.2 Extension-Under-Load Method**—Yield strength by the extension-under-load method may be determined by: (1) using autographic or numerical devices to secure stress-strain data, and then analyzing this data (graphically or using automated methods) to determine the stress value at the specified value of extension, or (2) using devices that indicate when the specified extension occurs, so that the stress then occurring may be ascertained (Note 27). Any of these devices



may be automatic. This method is illustrated in Fig. 22. The stress at the specified extension shall be reported as follows:

$$\text{yield strength (EUL = 0.5 \%)} = 52\,000 \text{ psi}$$

Extensometers and other devices used in determination of the extension shall meet Class B2 requirements (see Practice E 83) at the strain of interest, except where use of low-magnification Class C devices is helpful, such as in facilitating measurement of YPE, if observed. If Class C devices are used, this must be reported along with the results.

NOTE 24—The appropriate value of the total extension must be specified. For steels with nominal yield strengths of less than 80 000 psi, an appropriate value is 0.005 in./in. (0.5 %) of the gage length. For higher strength steels, a greater extension or the offset method should be used.

NOTE 25—When no other means of measuring elongation are available, a pair of dividers or similar device can be used to determine a point of detectable elongation between two gage marks on the specimen. The gage length shall be 2 in. The stress corresponding to the load at the instant of detectable elongation may be recorded as the *approximate extension-under-load yield strength*.

**7.5.3 Autographic Diagram Method (for materials exhibiting discontinuous yielding)**—Obtain stress-strain (or force elongation) data or construct a stress-strain (or load-elongation) diagram using an autographic device. Determine the upper or lower yield strength as follows:

7.5.3.1 Record the stress corresponding to the maximum force at the onset of discontinuous yielding as the upper yield strength. This is illustrated in Figs. 23 and 24.

NOTE 26—If multiple peaks are observed at the onset of discontinuous yielding, the first is considered the upper yield strength. (See Fig. 24.)

7.5.3.2 Record the minimum stress observed during discontinuous yielding (ignoring transient effects) as the lower yield strength. This is illustrated in Fig. 24.

NOTE 27—Yield properties of materials exhibiting yield point elongation are often less repeatable and less reproducible than those of similar materials having no YPE. Offset and EUL yield strengths may be significantly affected by force fluctuations occurring in the region where the offset or extension intersects the stress-strain curve. Determination of upper or lower yield strengths (or both) may therefore be preferable for such materials, although these properties are dependent on variables such as test machine stiffness and alignment. Speed of testing may also have a significant effect, regardless of the method employed.

NOTE 28—Where low-magnification autographic recordings are needed to facilitate measurement of yield point elongation for materials which may exhibit discontinuous yielding, Class C extensometers may be employed. When this is done but the material exhibits no discontinuous yielding, the extension-under-load yield strength may be determined instead, using the autographic recording (see Extension-Under-Load Method).

**7.5.4 Halt-of-the-Force Method (for materials exhibiting discontinuous yielding)**—Apply an increasing force to the specimen at a uniform deformation rate. When the force hesitates, record the corresponding stress as the upper yield strength.

NOTE 29—The Halt-of-the-Force Method was formerly known as the Halt-of-the-Pointer Method, the Drop-of-the-Beam Method, and the Halt-of-the-Load Method.

**7.5.5 Strain Rate Method (for materials that do not exhibit well-defined discontinuous yielding)**—Attach a Class B2 or better extensometer to the specimen at the gage marks. Increase the force at a reasonably uniform rate and watch the

elongation of the specimen as indicated by the extensometer. Note the force at which the rate of elongation suddenly increases.

**7.6 Yield Point Elongation**—Calculate the yield point elongation from the stress-strain diagram or data by determining the difference in strain between the upper yield strength (first zero slope) and the onset of uniform strain hardening (see definition of YPE and Fig. 24).

NOTE 30—The stress-strain curve of a material exhibiting only a hint of the behavior causing YPE may have an inflection at the onset of yielding with no point where the slope reaches zero (Fig. 25). Such a material has no YPE, but may be characterized as exhibiting an *inflection*. Materials exhibiting inflections, like those with measurable YPE, may in certain applications acquire an unacceptable surface appearance during forming.

**7.7 Tensile Strength**—Calculate the tensile strength by dividing the maximum force carried by the specimen during the tension test by the original cross-sectional area of the specimen.

NOTE 31—If the upper yield strength is the maximum stress recorded, and if the stress-strain curve resembles that of Fig. 26, it is recommended that the maximum stress *after discontinuous yielding* be reported as the tensile strength. Where this may occur, determination of the tensile strength should be in accordance with the agreement between the parties involved.

#### 7.8 Elongation:

7.8.1 In reporting values of elongation, give both the original gage length and the percentage increase. If any device other than an extensometer is placed in contact with the specimen's reduced section during the test, this also shall be noted.

Example: elongation = 30 % increase (2-in. gage length)

NOTE 32—Elongation results are very sensitive to variables such as: (a) speed of testing, (b) specimen geometry (gage length, diameter, width, and thickness), (c) heat dissipation (through grips, extensometers, or other devices in contact with the reduced section), (d) surface finish in reduced section (especially burrs or notches), (e) alignment, and (f) fillets and tapers. Parties involved in comparison or conformance testing should standardize the above items, and it is recommended that use of ancillary devices (such as extensometer supports) which may remove heat from specimens be avoided. See Appendix X1. for additional information on the effects of these variables.

7.8.2 When the specified elongation is greater than 3 %, fit ends of the fractured specimen together carefully and measure the distance between the gage marks to the nearest 0.01 in. for gage lengths of 2 in. and under, and to at least the nearest 0.5 % of the gage length for gage lengths over 2 in. A percentage scale reading to 0.5 % of the gage length may be used.

7.8.3 When the *specified* elongation is 3 % or less, determine the elongation of standard round specimens (see Fig. 8) using the following procedure, except that the procedure given in 7.8.2 may be used instead when the *measured* elongation is greater than 3 %.

7.8.3.1 Measure the original gage length of the specimen to the nearest 0.002 in.

7.8.3.2 Remove partly torn fragments that will interfere with fitting together the ends of the fractured specimen or with making the final measurement.

7.8.3.3 Fit the fractured ends together with matched surfaces and apply a force along the axis of the specimen sufficient to close the fractured ends together. If desired, this



force may then be removed carefully, provided the specimen remains intact.

NOTE 33—The use of a force of approximately 2000 psi has been found to give satisfactory results on test specimens of aluminum alloy.

7.8.3.4 Measure the final gage length to the nearest 0.002 in. and report the elongation to the nearest 0.2 %.

7.8.4 Specimens other than the standard specimen described in Fig. 8 are exempt from the requirement of 7.8.3 except as required by the applicable product specification.

7.8.5 If any part of the fracture takes place outside of the middle half of the gage length or in a punched or scribed mark within the reduced section, the elongation value obtained may not be representative of the material. In acceptance testing, if the elongation so measured meets the minimum requirements specified, no further testing is required, but if the elongation is less than the minimum requirements, discard the test and retest.

7.8.6 Elongation at fracture is defined as the elongation measured just prior to the sudden decrease in force associated with fracture. For many ductile materials not exhibiting a sudden decrease in force, the elongation at fracture can be taken as the strain measured just prior to when the force falls below 10 % of the maximum force encountered during the test.

7.8.6.1 Elongation at fracture shall include elastic and plastic elongation and may be determined with autographic or automated methods using extensometers. Use a class B2 or better extensometer for materials having less than 5 % elongation, a class C or better extensometer for materials having elongation greater than or equal to 5 % but less than 50 %, and a class D or better extensometer for materials having 50 % or greater elongation. In all cases, the extensometer gage length shall be the nominal gage length required for the specimen being tested. Due to the lack of precision in fitting fractured ends together, the elongation after fracture using the manual methods of the preceding paragraphs may differ from the elongation at fracture determined with extensometers.

7.8.6.2 Percent elongation at fracture may be calculated directly from elongation at fracture data and be reported instead of percent elongation as calculated in paragraphs 7.8.2 to 7.8.3. However, these two parameters are not interchangeable. Use of the elongation at fracture method generally provides more repeatable results.

NOTE 34—When disagreements arise over the percent elongation results, agreement must be reached on which method to use to obtain the results.

#### 7.9 Reduction of Area:

7.9.1 The reduced area used to calculate reduction of area (see 7.9.2 and 7.9.3) shall be the minimum cross section at the location of fracture.

7.9.2 *Specimens with Originally Circular Cross Sections*—Fit the ends of the fractured specimen together and measure the reduced diameter to the same accuracy as the original measurement.

NOTE 35—Because of anisotropy, circular cross sections often do not remain circular during straining in tension. The shape is usually elliptical, thus, the area may be calculated by  $\pi \cdot d_1 \cdot d_2/4$ , where  $d_1$  and  $d_2$  are the major and minor diameters, respectively.

7.9.3 *Specimens with Original Rectangular Cross Sec-*

*tions*—Fit the ends of the fractured specimen together and measure the thickness and width at the minimum cross section to the same accuracy as the original measurements.

NOTE 36—Because of the constraint to deformation that occurs at the corners of rectangular specimens, the dimensions at the center of the original flat surfaces are less than those at the corners. The shapes of these surfaces are often assumed to be parabolic. When this assumption is made, an effective thickness,  $t_e$ , may be calculated as follows:  $(t_1 + 4t_2 + t_3)/6$ , where  $t_1$  and  $t_3$  are the thicknesses at the corners, and  $t_2$  is the thickness at mid-width. An effective width may be similarly calculated.

7.9.4 Calculate the reduced area based upon the dimensions determined in 7.9.2 or 7.9.3. The difference between the area thus found and the area of the original cross section expressed as a percentage of the original area is the reduction of area.

7.9.5 If any part of the fracture takes place outside the middle half of the reduced section or in a punched or scribed gage mark within the reduced section, the reduction of area value obtained may not be representative of the material. In acceptance testing, if the reduction of area so calculated meets the minimum requirements specified, no further testing is required, but if the reduction of area is less than the minimum requirements, discard the test results and retest.

7.9.6 Results of measurements of reduction of area shall be rounded using the procedures of Practice E 29 and any specific procedures in the product specifications. In the absence of a specified procedure, it is recommended that reduction of area test values in the range from 0 to 10 % be rounded to the nearest 0.5 % and test values of 10 % and greater to the nearest 1 %.

7.10 *Rounding Reported Test Data for Yield Strength and Tensile Strength*—Test data should be rounded using the procedures of Practice E 29 and the specific procedures in the product specifications. In the absence of a specified procedure for rounding the test data, one of the procedures described in the following paragraphs is recommended.

7.10.1 For test values up to 50 000 psi, round to the nearest 100 psi; for test values of 50 000 psi and up to 100 000 psi, round to the nearest 500 psi; for test values of 100 000 psi and greater, round to the nearest 1000 psi.

NOTE 37—For steel products, see Test Methods and Definitions A 370.

7.10.2 For all test values, round to the nearest 100 psi.

NOTE 38—For aluminum- and magnesium-alloy products, see Methods B 557.

7.10.3 For all test values, round to the nearest 500 psi.

7.11 *Replacement of Specimens*—A test specimen may be discarded and a replacement specimen selected from the same lot of material in the following cases:

7.11.1 The original specimen had a poorly machined surface,

7.11.2 The original specimen had the wrong dimensions,

7.11.3 The specimen's properties were changed because of poor machining practice,

7.11.4 The test procedure was incorrect,

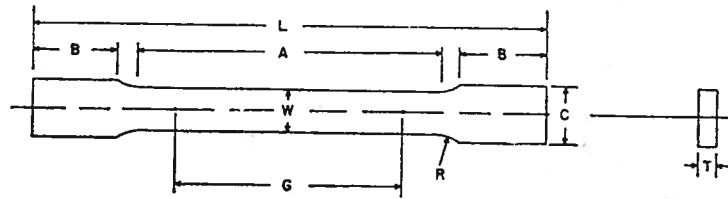
7.11.5 The fracture was outside the gage length,

7.11.6 For elongation determinations, the fracture was outside the middle half of the gage length, or

7.11.7 There was a malfunction of the testing equipment.



**E 8**



	Dimensions		
	Standard Specimens		Subsize Specimen
	Plate-Type, 1½-in. Wide	Sheet-Type, ½-in. Wide	¼-in. Wide
<i>G</i> —Gage length (Notes 1 and 2)	8.00 ± 0.01	2.000 ± 0.005	1.000 ± 0.003
<i>W</i> —Width (Notes 3 and 4)	1½ + ⅛, -¼	0.500 ± 0.010	0.250 ± 0.005
<i>T</i> —Thickness (Note 5)		thickness of material	
<i>R</i> —Radius of fillet, min (Note 6)	1	½	¼
<i>L</i> —Over-all length, min (Notes 2 and 7)	18	8	4
<i>A</i> —Length of reduced section, min	9	2¼	1¼
<i>B</i> —Length of grip section, min (Note 8)	3	2	1¼
<i>C</i> —Width of grip section, approximate (Notes 4 and 9)	2	¾	¾

NOTE 1—For the 1½-in. wide specimen, punch marks for measuring elongation after fracture shall be made on the flat or on the edge of the specimen and within the reduced section. Either a set of nine or more punch marks 1 in. apart, or one or more pairs of punch marks 8 in. apart may be used.

NOTE 2—When elongation measurements of 1½-in. wide specimens are not required, a minimum length of reduced section (*A*) of 2¼ in. may be used with all other dimensions similar to those of the plate-type specimen.

NOTE 3—For the three sizes of specimens, the ends of the reduced section shall not differ in width by more than 0.004, 0.002 or 0.001 in., respectively. Also, there may be a gradual decrease in width from the ends to the center, but the width at each end shall not be more than 0.015, 0.005, or 0.003 in., respectively, larger than the width at the center.

NOTE 4—For each of the three sizes of specimens, narrower widths (*W* and *C*) may be used when necessary. In such cases the width of the reduced section should be as large as the width of the material being tested permits; however, unless stated specifically, the requirements for elongation in a product specification shall not apply when these narrower specimens are used.

NOTE 5—The dimension *T* is the thickness of the test specimen as provided for in the applicable material specifications. Minimum thickness of 1½-in. wide specimens shall be ⅜ in. Maximum thickness of ½-in. and ¼-in. wide specimens shall be ¼ in. and ¼ in., respectively.

NOTE 6—For the 1½-in. wide specimen, a ½-in. minimum radius at the ends of the reduced section is permitted for steel specimens under 100 000 psi in tensile strength when a profile cutter is used to machine the reduced section.

NOTE 7—To aid in obtaining axial force application during testing of ¼-in. wide specimens, the over-all length should be as large as the material will permit, up to 8.00 in.

NOTE 8—It is desirable, if possible, to make the length of the grip section large enough to allow the specimen to extend into the grips a distance equal to two thirds or more of the length of the grips. If the thickness of ½-in. wide specimens is over ⅜ in., longer grips and correspondingly longer grip sections of the specimen may be necessary to prevent failure in the grip section.

NOTE 9—For the three sizes of specimens, the ends of the specimen shall be symmetrical in width with the center line of the reduced section within 0.10, 0.05 and 0.005 in., respectively. However, for referee testing and when required by product specifications, the ends of the ½-in. wide specimen shall be symmetrical within 0.01 in.

NOTE 10—For each specimen type, the radii of all fillets shall be equal to each other within a tolerance of 0.05 in., and the centers of curvature of the two fillets at a particular end shall be located across from each other (on a line perpendicular to the centerline) within a tolerance of 0.10 in.

NOTE 11—Specimens with sides parallel throughout their length are permitted, except for referee testing, provided: (a) the above tolerances are used; (b) an adequate number of marks are provided for determination of elongation; and (c) when yield strength is determined, a suitable extensometer is used. If the fracture occurs at a distance of less than 2*W* from the edge of the gripping device, the tensile properties determined may not be representative of the material. In acceptance testing, if the properties meet the minimum requirements specified, no further testing is required, but if they are less than the minimum requirements, discard the test and retest.

**FIG. 1 Rectangular Tension Test Specimens**

NOTE 39—The tension specimen is inappropriate for assessing some types of imperfections in a material. Other methods and specimens employing ultrasonics, dye penetrants, radiography, etc., may be considered when flaws such as cracks, flakes, porosity, etc., are revealed during a test and soundness is a condition of acceptance.

**8. Report**

8.1 Test information on materials not covered by a product specification should be reported in accordance with 8.2 or both 8.2 and 8.3.

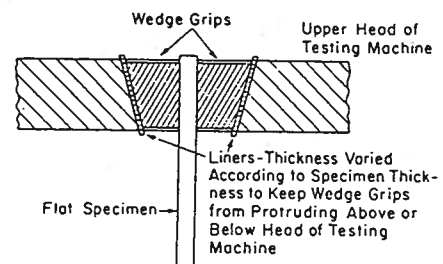
8.2 Test information to be reported shall include the following when applicable:

- 8.2.1 Material and sample identification.
- 8.2.2 Specimen type (see Section 6).
- 8.2.3 Yield strength and the method used to determine yield strength (see 7.5).
- 8.2.4 Yield point elongation (see 7.6).
- 8.2.5 Tensile strength (see 7.7).

8.2.6 Elongation (report original gage length, percentage increase, and method used to determine elongation) (see 7.8).

8.2.7 Reduction of area (see 7.9).

8.3 Test information to be available on request shall include:



**FIG. 2 Wedge Grips with Liners for Flat Specimens**

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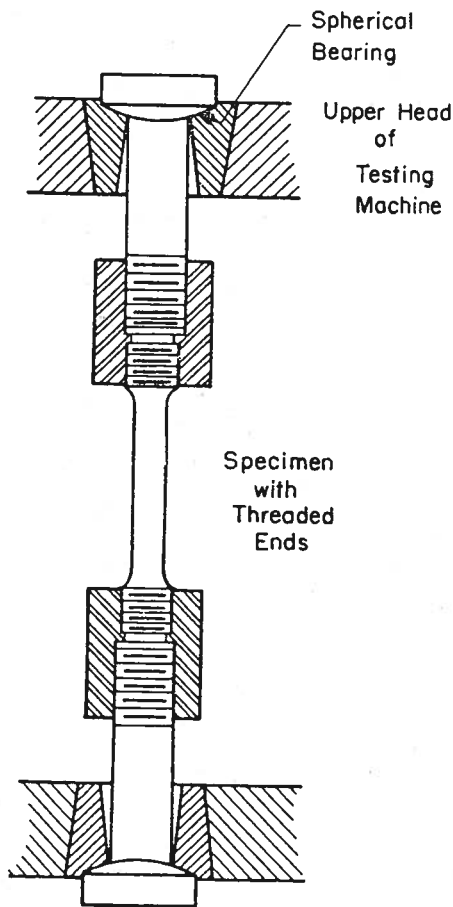


FIG. 3 Gripping Device for Threaded-End Specimens

- 8.3.1 Specimen test section dimension(s).
- 8.3.2 Equation used to calculate cross-sectional area of rectangular specimens taken from large-diameter tubular products.
- 8.3.3 Speed and method used to determine speed of testing (see 7.4).
- 8.3.4 Method used for rounding of test results (see 7.10).
- 8.3.5 Reasons for replacement specimens (see 7.11).

9. Precision and Bias

9.1 Precision—An interlaboratory test program<sup>7</sup> gave the following values for coefficients of variation for the most commonly measured tensile properties:

	Coefficient of Variation, %				
	Tensile Strength	Yield Strength Offset= 0.02 %	Yield Strength Offset= 0.2 %	Elongation Gage Length= 4 Diameter	Reduction of Area
CV % <sub>r</sub>	0.9	2.7	1.4	2.8	2.8
CV % <sub>R</sub>	1.3	4.5	2.3	5.4	4.6

CV %<sub>r</sub> = repeatability coefficient of variation in percent within a laboratory  
 CV %<sub>R</sub> = repeatability coefficient of variation in percent between laboratories

9.1.1 The values shown are the averages from tests on six

<sup>7</sup> Supporting data can be found in Appendix I and additional data are available from ASTM Headquarters. Request RR: E28-1004.

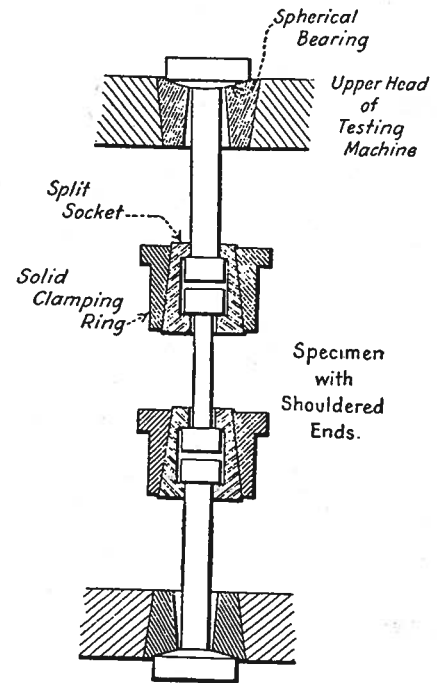


FIG. 4 Gripping Device for Shouldered-End Specimens

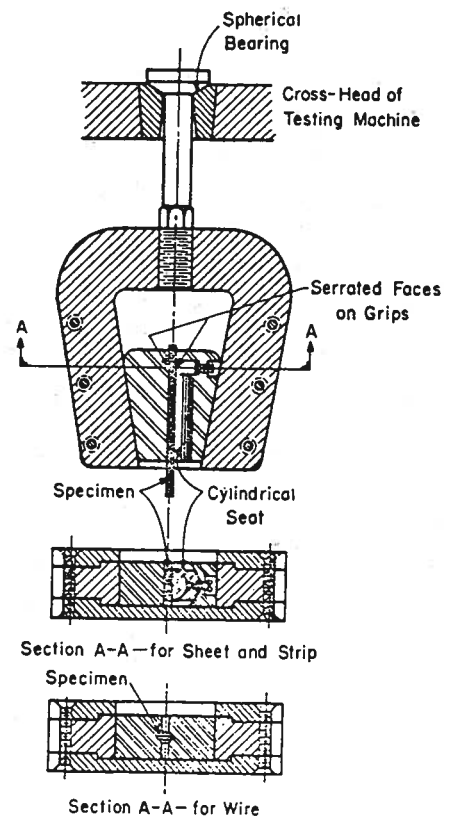


FIG. 5 Gripping Devices for Sheet and Wire Specimens

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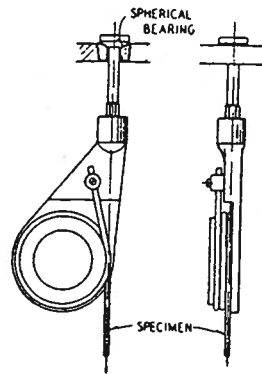
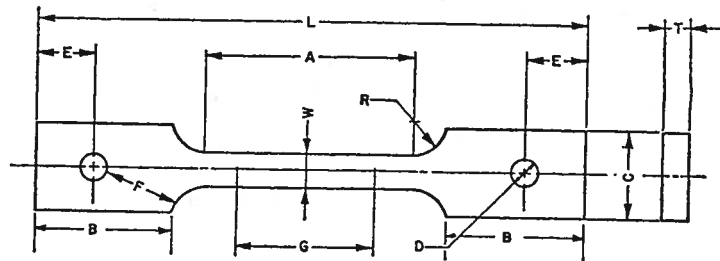


FIG. 6 Snubbing Device for Testing Wire



Dimensions	in.
G—Gage length	2.000 ± 0.005
W—Width (Note 1)	0.500 ± 0.010
T—Thickness, max (Note 2)	5/8
R—Radius of fillet, min (Note 3)	1/2
L—Over-all length, min	8
A—Length of reduced section, min	2 1/4
B—Length of grip section, min	2
C—Width of grip section, approximate	2
D—Diameter of hole for pin, min (Note 4)	1/2
E—Edge distance from pin, approximate	1 1/2
F—Distance from hole to fillet, min	1/2

NOTE 1—The ends of the reduced section shall differ in width by not more than 0.002 in. There may be a gradual taper in width from the ends to the center, but the width at each end shall be not more than 0.005 in. greater than the width at the center.

NOTE 2—The dimension T is the thickness of the test specimen as stated in the applicable product specifications.

NOTE 3—For some materials, a fillet radius R larger than 1/2 in. may be needed.

NOTE 4—Holes must be on center line of reduced section, within ±0.002 in.

NOTE 5—Variations of dimensions C, D, E, F, and L may be used that will permit failure within the gage length.

FIG. 7 Pin-Loaded Tension Test Specimen with 2-in. Gage Length

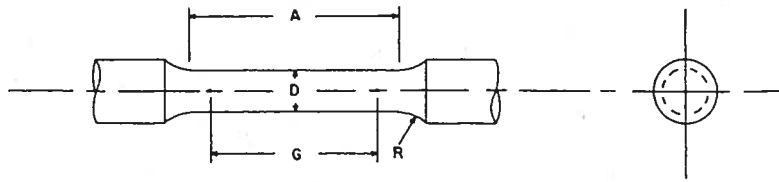
frequently tested metals, selected to include most of the normal range for each property listed above. When these materials are compared, a large difference in coefficient of variation is found. Therefore, the values above should not be used to judge whether the difference between duplicate tests of a specific material is larger than expected. The values are provided to allow potential users of this test method to assess, in general terms, its usefulness for a proposed application.

9.2 Bias—The procedures in Test Methods E 8 for measuring tensile properties have no bias because these properties can be defined only in terms of a test method.

## 10. Keywords

10.1 accuracy; bending stress; discontinuous yielding; drop-of-the-beam; eccentric force application; elastic extension; elongation; extension-under-load; extensometer; force; free-running crosshead speed; gage length; half-of-the force; percent elongation; plastic extension; preload; rate of stressing; rate of straining; reduced section; reduction of area; sensitivity; strain; stress; taring; tensile strength; tension testing; yield point elongation; yield strength

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Nominal Diameter	Dimensions				
	Standard Specimen		Small-Size Specimens Proportional to Standard		
	in.	in.	in.	in.	in.
0.500	0.350	0.250	0.160	0.113	
G—Gage length	2.000 ± 0.005	1.400 ± 0.005	1.000 ± 0.005	0.640 ± 0.005	0.450 ± 0.005
D—Diameter (Note 1)	0.500 ± 0.010	0.350 ± 0.007	0.250 ± 0.005	0.160 ± 0.003	0.113 ± 0.002
R—Radius of fillet, min	3/8	1/4	3/16	5/32	3/32
A—Length of reduced section, min (Note 2)	2 1/4	1 3/4	1 1/4	3/4	5/8

NOTE 1—The reduced section may have a gradual taper from the ends toward the center, with the ends not more than 1 % larger in diameter than the center (controlling dimension).

NOTE 2—If desired, the length of the reduced section may be increased to accommodate an extensometer of any convenient gage length. Reference marks for the measurement of elongation should, nevertheless, be spaced at the indicated gage length.

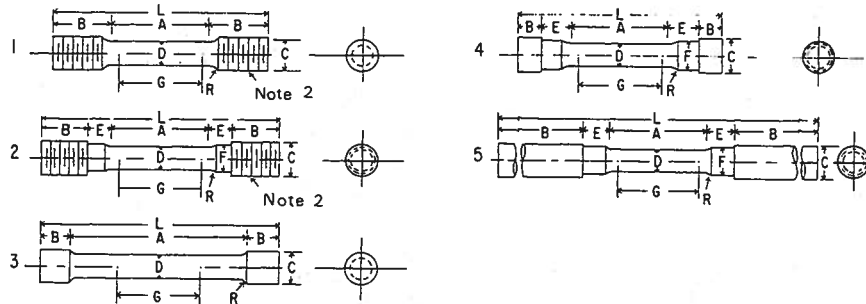
NOTE 3—The gage length and fillets may be as shown, but the ends may be of any form to fit the holders of the testing machine in such a way that the load shall be axial (see Fig. 9). If the ends are to be held in wedge grips it is desirable, if possible, to make the length of the grip section great enough to allow the specimen to extend into the grips a distance equal to two thirds or more of the length of the grips.

NOTE 4—On the round specimens in Figs. 8 and 9, the gage lengths are equal to four times the nominal diameter. In some product specifications other specimens may be provided for, but unless the 4-to-1 ratio is maintained within dimensional tolerances, the elongation values may not be comparable with those obtained from the standard test specimen.

NOTE 5—The use of specimens smaller than 0.250-in. diameter shall be restricted to cases when the material to be tested is of insufficient size to obtain larger specimens or when all parties agree to their use for acceptance testing. Smaller specimens require suitable equipment and greater skill in both machining and testing.

NOTE 6—Five sizes of specimens often used have diameters of approximately 0.505, 0.357, 0.252, 0.160, and 0.113 in., the reason being to permit easy calculations of stress from loads, since the corresponding cross-sectional areas are equal or close to 0.200, 0.100, 0.0500, 0.0200, and 0.0100 in.<sup>2</sup>, respectively. Thus, when the actual diameters agree with these values, the stresses (or strengths) may be computed using the simple multiplying factors 5, 10, 20, 50, and 100, respectively. (The metric equivalents of these five diameters do not result in correspondingly convenient cross-sectional areas and multiplying factors.)

**FIG. 8 Standard 0.500-in. Round Tension Test Specimen with 2-in. Gage Length and Examples of Small-Size Specimens Proportional to the Standard Specimen**



	Dimensions				
	Specimen 1	Specimen 2	Specimen 3	Specimen 4	Specimen 5
	in.	in.	in.	in.	in.
G—Gage length	2.000 ± 0.005	2.000 ± 0.005	2.000 ± 0.005	2.000 ± 0.005	2.000 ± 0.005
D—Diameter (Note 1)	0.500 ± 0.010	0.500 ± 0.010	0.500 ± 0.010	0.500 ± 0.010	0.500 ± 0.010
R—Radius of fillet, min	3/8	3/8	1/16	3/8	3/8
A—Length of reduced section	2 1/4, min	2 1/4, min	4, approximately	2 1/4, min	2 1/4, min
L—Over-all length, approximate	5	5 1/2	5 1/2	4 3/4	9 1/2
B—Length of end section (Note 3)	1 3/8, approximately	1, approximately	3/4, approximately	1/2, approximately	3, min
C—Diameter of end section	3/4	3/4	23/32	7/8	3/4
E—Length of shoulder and fillet section, approximate	...	5/8	...	3/4	5/8
F—Diameter of shoulder	...	5/8	...	5/8	1 1/32

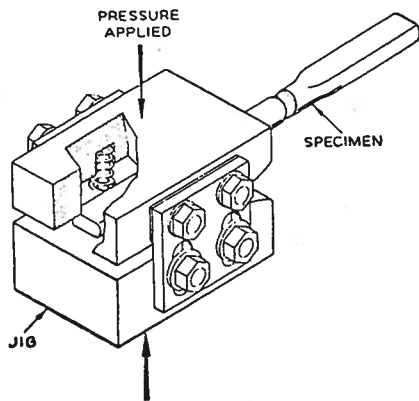
NOTE 1—The reduced section may have a gradual taper from the ends toward the center with the ends not more than 0.005 in. larger in diameter than the center.

NOTE 2—On Specimens 1 and 2, any standard thread is permissible that provides for proper alignment and aids in assuring that the specimen will break within the reduced section.

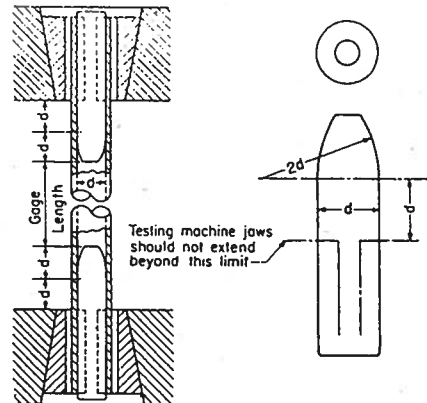
NOTE 3—On Specimen 5 it is desirable, if possible, to make the length of the grip section great enough to allow the specimen to extend into the grips a distance equal to two thirds or more of the length of the grips.

**FIG. 9 Various Types of Ends for Standard Round Tension Test Specimens**

**E 8**

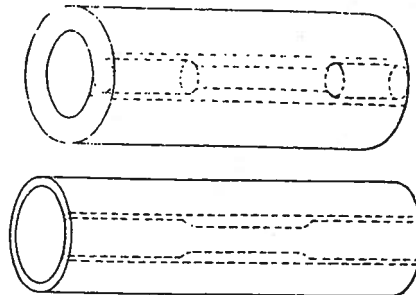


**FIG. 10 Squeezing Jig for Flattening Ends of Full-Size Tension Test Specimens**



NOTE—The diameter of the plug shall have a slight taper from the line limiting the test machine jaws to the curved section.

**FIG. 11 Metal Plugs for Testing Tubular Specimens, Proper Location of Plugs in Specimen and of Specimen in Heads of Testing Machine**

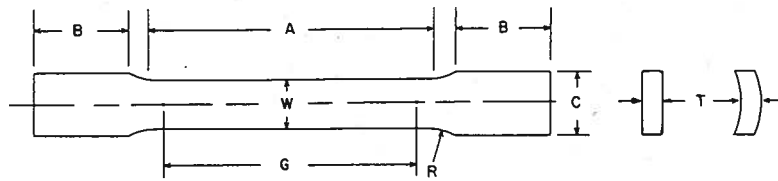


NOTE—The edges of the blank for the specimen shall be cut parallel to each other.

**FIG. 12 Location from Which Longitudinal Tension Test Specimens Are to be Cut from Large-Diameter Tube**



**E 8**



	Dimensions						
	Specimen 1	Specimen 2	Specimen 3	Specimen 4	Specimen 5	Specimen 6	Specimen 7
	in.	in.	in.	in.	in.	in.	in.
G—Gage length	2.000 ± 0.005	2.000 ± 0.005	8.00 ± 0.01	2.000 ± 0.005	4.000 ± 0.005	2.000 ± 0.005	4.000 ± 0.005
W—Width (Note 1)	0.500 ± 0.010	1½ + ¼, -¼	1½ + ¼, -¼	0.750 ± 0.031	0.750 ± 0.031	1.000 ± 0.062	1.000 ± 0.062
T—Thickness	measured thickness of specimen						
R—Radius of fillet, min	½	1	1	1	1	1	1
A—Length of reduced section, min	2¼	2¼	9	2¼	4½	¼	4½
B—Length of grip section, min (Note 2)	3	3	3	3	3	3	3
C—Width of grip section, approximate (Note 3)	1⅞	2	2	1	1	1½	1½

NOTE 1—The ends of the reduced section shall differ in width by not more than 0.002 in. for specimens 1 and 4, and not more than 0.005 in. for specimens 2, 3, 5, 6, and 7. There may be a gradual taper in width from the ends to the center, but the width at each end shall be not more than 0.005 in. greater than the width at the center for 2-in. gage length specimens, not more than 0.008 in. greater than the width at the center for 4-in. gage length specimens, and not more than 0.015 in. greater than the width at the center for 8-in. gage length specimens.

NOTE 2—It is desirable, if possible, to make the length of the grip section great enough to allow the specimen to extend into the grips a distance equal to two thirds or more of the length of the grips.

NOTE 3—The ends of the specimen shall be symmetrical with the center line of the reduced section within 0.05 in. for specimens 1, 4, and 5, and 0.10 in. for specimens 2, 3, 6, and 7.

NOTE 4—For each specimen type, the radii of all fillets shall be equal to each other within a tolerance of 0.05 in., and the centers of curvature of the two fillets at a particular end shall be located across from each other (on a line perpendicular to the centerline) within a tolerance of 0.10 in.

NOTE 5—For circular segments, the cross-sectional area may be calculated by multiplying W and T. If the ratio of the dimension W to the diameter of the tubular section is larger than about ¼, the error in using this method to calculate the cross-sectional area may be appreciable. In this case, the exact equation (see 7.1.3) must be used to determine the area.

NOTE 6—Specimens with G/W less than 4 should not be used for determination of elongation.

NOTE 7—Specimens with sides parallel throughout their length are permitted, except for referee testing, provided: (a) the above tolerances are used; (b) an adequate number of marks are provided for determination of elongation; and (c) when yield strength is determined, a suitable extensometer is used. If the fracture occurs at a distance of less than 2W from the edge of the gripping device, the tensile properties determined may not be representative of the material. If the properties meet the minimum requirements specified, no further testing is required, but if they are less than the minimum requirements, discard the test and retest.

FIG. 13 Tension Test Specimens for Large-Diameter Tubular Products

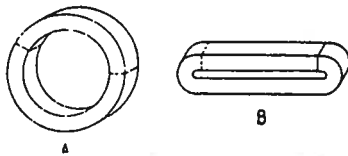
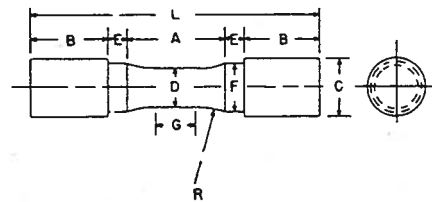


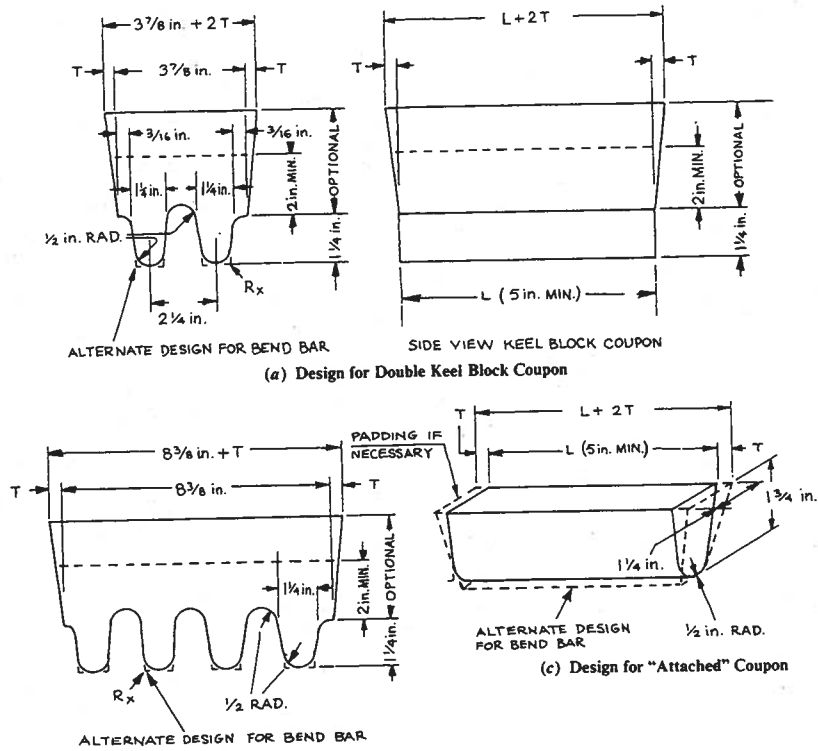
FIG. 14 Location of Transverse Tension Test Specimen in Ring Cut from Tubular Products

	Dimensions		
	Specimen 1	Specimen 2	Specimen 3
	in.	in.	in.
G—Length of parallel section	Shall be equal to or greater than diameter D		
D—Diameter	0.500 ± 0.010	0.750 ± 0.015	1.25 ± 0.02
R—Radius of fillet, min	1	1	2
A—Length of reduced section, min	1¼	1½	2¼
L—Over-all length, min	3¾	4	6¾
B—Length of end section, approximate	1	1	1¾
C—Diameter of end section, approximate	¾	1⅞	1⅞
E—Length of shoulder, min	¼	¼	5/16
F—Diameter of shoulder	5/8 ± 1/64	19/16 ± 1/64	17/16 ± 1/64

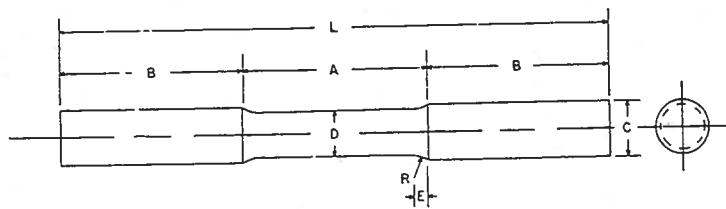
NOTE—The reduced section and shoulders (dimensions A, D, E, F, G, and R) shall be as shown, but the ends may be of any form to fit the holders of the testing machine in such a way that the force can be axial. Commonly the ends are threaded and have the dimensions B and C given above.

FIG. 15 Standard Tension Test Specimen for Cast Iron

**E 8**



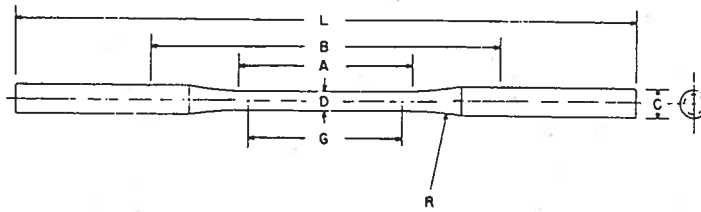
**FIG. 16 Test Coupons for Castings (see Table 1 for Details of Design)**



Dimensions		in.
D—Diameter		9/8
R—Radius of fillet		5/16
A—Length of reduced section		2 1/2
L—Over-all length		7 1/2
B—Length of end section		2 1/2
C—Diameter of end section		3/4
E—Length of fillet		3/16

**FIG. 17 Standard Tension Test Specimen for Malleable Iron**

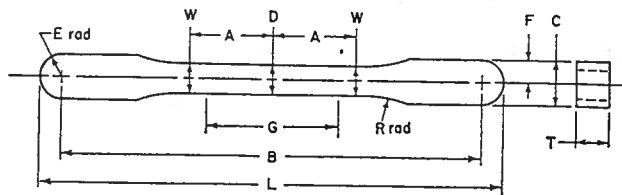
**E 8**



Dimensions		in.
G—Gage length		2.000 ± 0.005
D—Diameter (see Note)		0.250 ± 0.005
R—Radius of fillet, min.		3
A—Length of reduced section, min.		2 1/4
L—Over-all length, min.		9
B—Distance between grips, min.		4 1/2
C—Diameter of end section, approximate		3/8

NOTE—The reduced section may have a gradual taper from the ends toward the center, with the ends not more than 0.005 in. larger in diameter than the center.

**FIG. 18 Standard Tension Test Specimens for Die Castings**

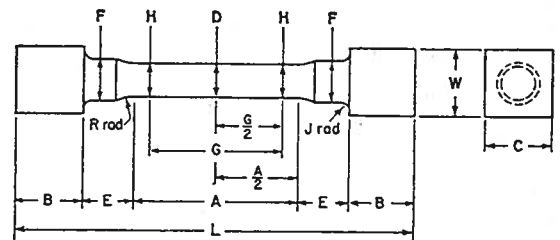


Pressing Area = 1.00 in.<sup>2</sup>

Dimensions		in.
G—Gage length		1.000 ± 0.003
D—Width at center		0.225 ± 0.001
W—Width at end of reduced section		0.235 ± 0.001
T—Compact to this thickness		0.140 to 0.250
R—Radius of fillet		1
A—Half-length of reduced section		5/8
B—Grip length		3.187 ± 0.001
L—Overall length		3.529 ± 0.001
C—Width of grip section		0.343 ± 0.001
F—Half-width of grip section		0.171 ± 0.001
E—End radius		0.171 ± 0.001

NOTE—Dimensions Specified, except G and T, are those of the die.

**FIG. 19 Standard Flat Unmachined Tension Test Specimens for Powder Metallurgy (P/M) Products**



Approximate Pressing Area of Unmachined Compact = 1.166 in.<sup>2</sup>  
Machining Recommendations

1. Rough machine reduced section to 1/4 -in. diameter
2. Finish turn 0.187/0.191-in. diameter with radii and taper
3. Polish with 00 emery cloth
4. Lap with crocus cloth

Dimensions		in.
G—Gage length		1.000 ± 0.003
D—Diameter at center of reduced section		0.187 ± 0.001
H—Diameter at ends of gage length		0.191 ± 0.001
R—Radius of fillet		0.250 ± 0.005
A—Length of reduced section		1.875 ± 0.003
L—Overall length (die cavity length)		3, nominal
B—Length of end section		0.310 ± 0.005
C—Compact to this end thickness		0.395 ± 0.005
W—Die cavity width		0.395 ± 0.003
E—Length of shoulder		0.250 ± 0.005
F—Diameter of shoulder		0.310 ± 0.001
J—End fillet radius		0.050 ± 0.005

NOTE 1—The gage length and fillets of the specimen shall be as shown. The ends as shown are designed to provide a practical minimum pressing area. Other end designs are acceptable, and in some cases are required for high-strength sintered materials.

NOTE 2—It is recommended that the test specimen be gripped with a split collet and supported under the shoulders. The radius of the collet support circular edge is to be not less than the end fillet radius of the test specimen.

NOTE 3—Diameters D and H are to be concentric within 0.001 in. total indicator runoff (T.I.R.), and free of scratches and tool marks.

**FIG. 20 Standard Round Machined Tension Test Specimen for Powder Metallurgy (P/M) Products**

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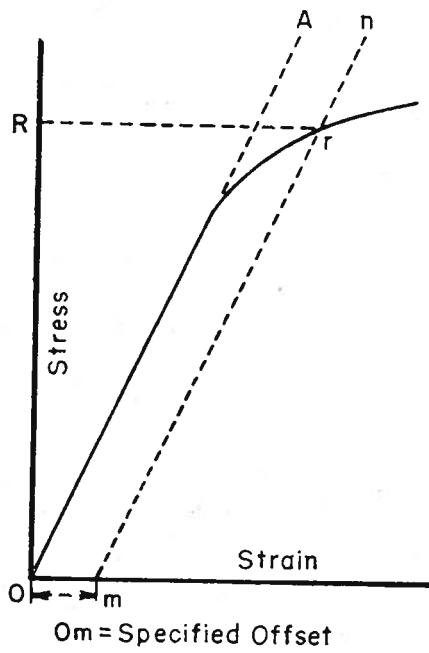


FIG. 21 Stress-Strain Diagram for Determination of Yield Strength by the Offset Method

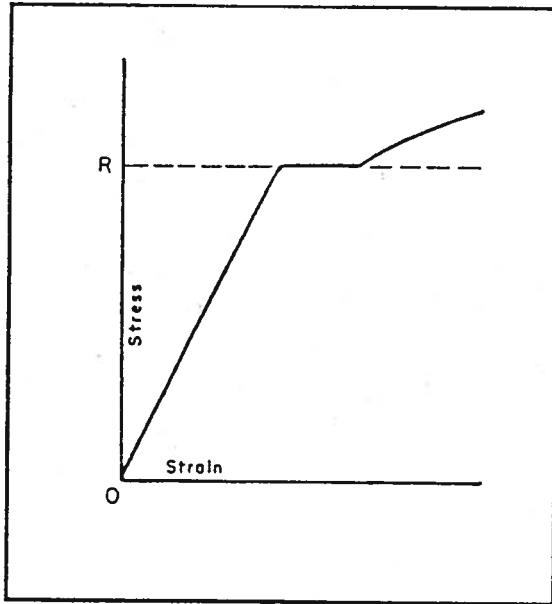


FIG. 23 Stress-Strain Diagram Showing Upper Yield Strength Corresponding with Top of Knee

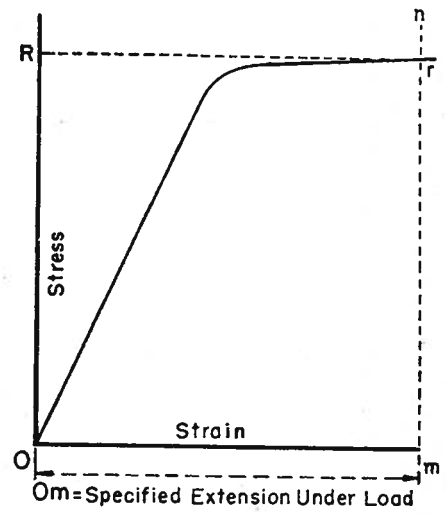


FIG. 22 Stress-Strain Diagram for Determination of Yield Strength by the Extension-Under-Load Method

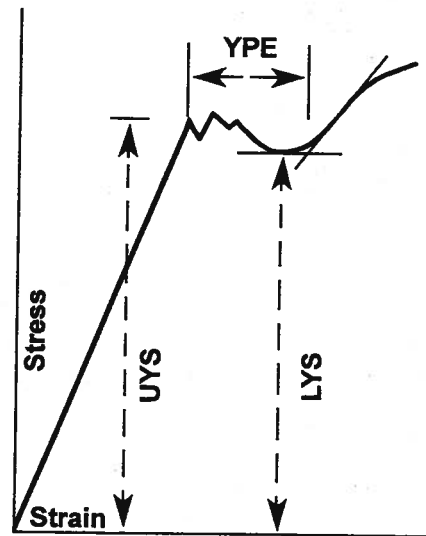


FIG. 24 Stress-Strain Diagram Showing Yield Point Elongation and Upper and Lower Yield Strengths

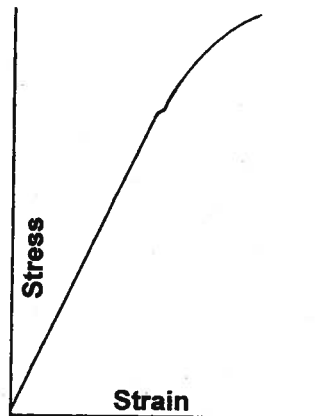


FIG. 25 Stress-Strain Diagram With an Inflection, But No YPE

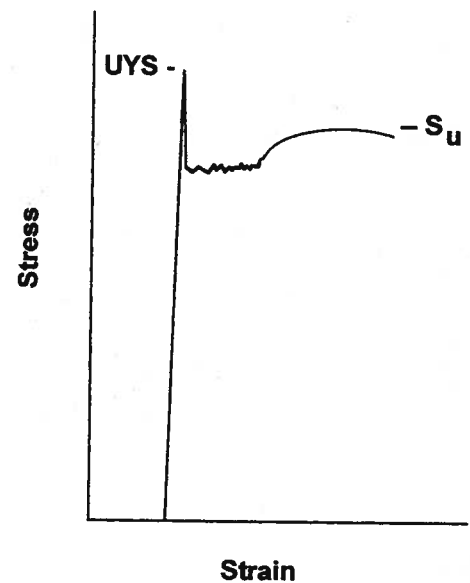


FIG. 26 Stress-Strain Diagram in Which the Upper Yield Strength is the Maximum Stress Recorded

## APPENDIXES

(Nonmandatory Information)

### X1. FACTORS AFFECTING TENSION TEST RESULTS

X1.1 The precision and bias of tension test strength and ductility measurements depend on strict adherence to the stated test procedure and are influenced by instrumental and material factors, specimen preparation, and measurement/testing errors.

X1.2 The consistency of agreement for repeated tests of the same material is dependent on the homogeneity of the material, and the repeatability of specimen preparation, test conditions, and measurements of the tension test parameters.

X1.3 Instrumental factors that can affect test results include: the stiffness, damping capacity, natural frequency, and mass of moving parts of the tensile test machine; accuracy of force indication and use of forces within the verified range of the machine; rate of force application, alignment of the test specimen with the applied force, parallelness of the grips, grip pressure, nature of the force control used, appropriateness and calibration of extensometers, heat dissipation (by grips, extensometers, or ancillary devices), and so forth.

X1.4 Material factors that can affect test results include: representativeness and homogeneity of the test material, sampling scheme, and specimen preparation (surface finish, dimensional accuracy, fillets at the ends of the gage length, taper in the gage length, bent specimens, thread quality, and so forth).

X1.4.1 Some materials are very sensitive to the quality of the surface finish of the test specimen (see Note 12) and must

be ground to a fine finish, or polished to obtain correct results.

X1.4.2 Test results for specimens with as-cast, as-rolled, as-forged, or other non-machined surface conditions can be affected by the nature of the surface (see Note 14).

X1.4.3 Test specimens taken from appendages to the part or component, such as prolongs or risers, or from separately produced castings (for example, keel blocks) may produce test results that are not representative of the part or component.

X1.4.4 Test specimen dimensions can influence test results. For cylindrical or rectangular specimens, changing the test specimen size generally has a negligible effect on the yield and tensile strength but may influence the upper yield strength, if one is present, and elongation and reduction of area values. Comparison of elongation values determined using different specimens requires that the following ratio be controlled:

$$L_o/(A_o)^{1/2}$$

where:

$L_o$  = original gage length of specimen, and  
 $A_o$  = original cross-sectional area of specimen.

X1.4.4.1 Specimens with smaller  $L_o/(A_o)^{1/2}$  ratios generally give greater elongation and reduction in area values. This is the case for example, when the width or thickness of a rectangular tensile test specimen is increased.

X1.4.4.2 Holding the  $L_o/(A_o)^{1/2}$  ratio constant minimizes, but does not necessarily eliminate, differences. Depending



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on material and test conditions, increasing the size of the proportional specimen of Fig. 8 may be found to increase or decrease elongation and reduction in area values somewhat.

X1.4.5 Use of a taper in the gage length, up to the allowed 1 % limit, can result in lower elongation values. Reductions of as much as 15 % have been reported for a 1 % taper.

X1.4.6 Some materials are highly strain-rate sensitive. Changes in the strain rate can affect the yield strength and elongation values, especially for strain-rate sensitive materials. In general, the yield strength and elongation will increase as the strain rate increases.

X1.4.7 Brittle materials require careful specimen preparation, high quality surface finishes, large fillets at the ends of the gage length, oversize threaded grip sections, and cannot

tolerate punch or scribe marks as gage length indicators.

X1.4.8 Flattening of tubular products to permit testing does alter the material properties, generally nonuniformly, in the flattened region which may affect test results.

X1.5 Measurement errors that can affect test results include: verification of the test force, extensometers, micrometers, dividers, and other measurement devices, alignment and zeroing of chart recording devices, and so forth.

X1.5.1 Measurement of the dimensions of as-cast, as-rolled, as-forged, and other test specimens with non-machined surfaces may be imprecise due to the irregularity of the surface flatness.

X1.5.2 Materials with anisotropic flow characteristics may exhibit non-circular cross sections after fracture and

**TABLE X1.1 Precision Statistics—Tensile Strength, ksi**

Material	X	s <sub>r</sub>	s <sub>r</sub> /X, %	s <sub>R</sub>	s <sub>R</sub> /X, %	r	R
EC-H19	25.66	0.63	2.45	0.63	2.45	1.76	1.76
2024-T351	71.26	0.88	1.24	0.96	1.34	2.47	2.68
ASTM A105	86.57	0.60	0.70	1.27	1.46	1.68	3.55
AISI 316	100.75	0.39	0.39	1.21	1.20	1.09	3.39
Inconel 600	99.48	0.42	0.43	0.72	0.72	1.19	2.02
SAE 51410	181.73	0.46	<u>0.25</u>	1.14	<u>0.63</u>	1.29	3.20
Averages:			0.91		1.30		

NOTE: X is the average of the cell averages, that is, the grand mean for the test parameter,  
s<sub>r</sub> is the repeatability standard deviation (within-laboratory precision),  
s<sub>r</sub>/X is the coefficient of variation in %,  
s<sub>R</sub> is the reproducibility standard deviation (between-laboratory precision),  
s<sub>R</sub>/X is the coefficient of variation, %,  
r is the 95 % repeatability limits,  
R is the 95 % reproducibility limits.

**TABLE X1.2 Precision Statistics—0.02 % Yield Strength, ksi**

Material	X	s <sub>r</sub>	s <sub>r</sub> /X, %	s <sub>R</sub>	s <sub>R</sub> /X, %	r	R
EC-H19	16.17	0.65	3.99	1.19	7.36	1.81	3.33
2024-T351	51.38	0.84	1.64	0.89	1.73	2.36	2.49
ASTM A105	59.66	1.20	2.02	1.89	3.18	3.37	5.31
AISI 316	48.62	2.39	4.91	4.61	9.49	6.68	12.91
Inconel 600	38.74	0.46	1.18	0.76	1.96	1.28	2.13
SAE 15410	104.90	2.40	<u>2.29</u>	3.17	<u>3.02</u>	6.73	8.88
Averages:			2.67		4.46		

**TABLE X1.3 Precision Statistics—0.2 % Yield Strength, ksi**

Material	X	s <sub>r</sub>	s <sub>r</sub> /X, %	s <sub>R</sub>	s <sub>R</sub> /X, %	r	R
EC-H19	22.98	0.47	2.06	0.48	2.07	1.33	1.33
2024-T351	52.64	0.74	1.41	0.79	1.49	2.08	2.20
ASTM A105	58.36	0.83	1.42	1.44	2.47	2.31	4.03
AISI 316	69.63	0.94	1.35	2.83	4.07	2.63	7.93
Inconel 600	38.91	0.36	0.93	0.85	2.18	1.01	2.37
SAE 51410	140.33	1.29	<u>0.92</u>	2.30	<u>1.64</u>	3.60	6.45
Averages:			1.35		2.32		

**TABLE X1.4 Precision Statistics—% Elongation in 4D**

Material	X	s <sub>r</sub>	s <sub>r</sub> /X, %	s <sub>R</sub>	s <sub>R</sub> /X, %	r	R
EC-H19	17.45	0.64	3.69	0.92	5.30	1.80	2.59
2024-T351	19.75	0.59	2.99	1.58	8.00	1.65	4.43
ASTM A105	29.10	0.76	2.62	0.98	3.38	2.13	2.76
AISI 316	40.07	1.10	2.75	2.14	5.35	3.09	6.00
Inconel 600	44.27	0.66	1.50	1.54	3.48	1.86	4.31
SAE 51410	14.48	0.48	<u>3.29</u>	0.99	<u>6.83</u>	1.34	2.77
Averages:			2.81		5.39		

NOTE A1—Length of reduced section = 6D.



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TABLE X1.5 Precision Statistics—% Reduction in Area

Material	X	$s_r$	$s_r/X, \%$	$s_R$	$s_R/X, \%$	r	R
EC-H19	79.14	1.94	2.45	2.02	2.56	5.44	5.67
2024-T351	30.31	2.07	6.82	3.58	11.80	5.79	10.01
ASTM A105	65.59	0.84	1.28	1.26	1.92	2.35	3.53
AISI 316	71.49	0.99	1.39	1.61	2.25	2.78	4.50
Inconel 600	59.34	0.67	1.14	0.70	1.18	1.89	1.97
SAE 51410	50.49	1.86	3.69	3.95	7.81	5.21	11.05
		Averages:	2.80		4.59		

measurement precision may be affected, as a result (see Note 35).

X1.5.3 The corners of rectangular test specimens are subject to constraint during deformation and the originally flat surfaces may be parabolic in shape after testing which will affect the precision of final cross-sectional area measurements (see Note 36).

X1.5.4 If any portion of the fracture occurs outside of the middle of the gage length, or in a punch or scribe mark within the gage length, the elongation and reduction of area values may not be representative of the material. Wire specimens that break at or within the grips may not produce test results representative of the material.

X1.5.5 Use of specimens with shouldered ends ("button-head" tensiles) will produce lower 0.02 % offset yield strength values than threaded specimens.

X1.6 Because standard reference materials with certified tensile property values are not available, it is not possible to rigorously define the bias of tension tests. However, by the use of carefully designed and controlled interlaboratory studies, a reasonable definition of the precision of tension test results can be obtained.

X1.6.1 An interlaboratory test program<sup>7</sup> was conducted in which six specimens each, of six different materials were prepared and tested by each of six different laboratories. Tables X1.1 to X1.5 present the precision statistics, as defined in Practice E 691, for: tensile strength, 0.02 % yield strength, 0.2 % yield strength, % elongation in 4D, and % reduction in area. In each table, the first column lists the six materials tested, the second column lists the average of the

average results obtained by the laboratories, the third and fifth columns list the repeatability and reproducibility standard deviations, the fourth and sixth columns list the coefficients of variation for these standard deviations, and the seventh and eighth columns list the 95 % repeatability and reproducibility limits.

X1.6.2 The averages (below columns four and six in each table) of the coefficients of variation permit a relative comparison of the repeatability (within-laboratory precision) and reproducibility (between-laboratory precision) of the tension test parameters. This shows that the ductility measurements exhibit less repeatability and reproducibility than the strength measurements. The overall ranking from the least to the most repeatable and reproducible is: % elongation in 4D, % reduction in area, 0.02 % offset yield strength, 0.2 % offset yield strength, and tensile strength. Note that the rankings are in the same order for the repeatability and reproducibility average coefficients of variation and that the reproducibility (between-laboratory precision) is poorer than the repeatability (within-laboratory precision), as would be expected.

X1.6.3 No comments about bias can be made for the interlaboratory study due to the lack of certified test results for these specimens. However, examination of the test results showed that one laboratory consistently exhibited higher than average strength values and lower than average ductility values for most of the specimens. One other laboratory had consistently lower than average tensile strength results for all specimens.

## X2. MEASUREMENT OF SPECIMEN DIMENSIONS

X2.1 Measurement of specimen dimensions is critical in tension testing, and it becomes more critical with decreasing specimen size, as a given absolute error becomes a larger relative (percent) error. Measuring devices and procedures should be selected carefully, so as to minimize measurement error and provide good repeatability and reproducibility.

X2.2 Relative measurement error should be kept at or below 1 %, where possible. Ideally, this 1 % error should include not only the resolution of the measuring device but also the variability commonly referred to as repeatability and reproducibility. (Repeatability is the ability of any operator to obtain similar measurements in repeated trials. Reproducibility is the ability of multiple operators to obtain similar measurements.)

X2.3 Formal evaluation of gage repeatability and reproducibility (GR and R) by way of a GR and R study is highly recommended. A GR and R study involves having multiple operators each take two or three measurements of a number

of parts—in this case, test specimens. Analysis, usually done by computer, involves comparing the observed measurement variations to a tolerance the procedure is to determine conformance to. High GR and R percentages (more than 20 %) indicate much variability relative to the tolerance whereas low percentages (10 % or lower) indicate the opposite. The analysis also estimates, independently, the repeatability and reproducibility.

X2.4 GR and R studies in which nontechnical personnel used different brands and models of hand-held micrometers have given results varying from about 10 % (excellent) to nearly 100 % (essentially useless), relative to a dimensional tolerance of 0.003 in. The user is therefore advised to be very careful in selecting devices, setting up measurement procedures, and training personnel.

X2.5 With a 0.003 in. tolerance, a 10 % GR and R result (exceptionally good, even for digital hand-held micrometers reading to 0.00005 in.) indicates that the total variation due



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to repeatability and reproducibility is around 0.0003 in. This is less than or equal to 1 % only if all dimensions to be measured are greater than or equal to 0.03 in. The relative error in using this device to measure thickness of a 0.01 in. flat tensile specimen would be 3 %—which is considerably more than that allowed for load or strain measurement.

X2.6 Dimensional measurement errors can be identified as the cause of many *out-of-control* signals, as indicated by statistical process control (SPC) charts used to monitor tension testing procedures. This has been the experience of a production laboratory employing SPC methodology and the best hand-held micrometers available (from a GR and R standpoint) in testing of 0.018 in. to 0.25 in. flat rolled steel products.

X2.7 Factors which affect GR and R, sometimes dramatically, and which should be considered in the selection and evaluation of hardware and procedures include:

X2.7.1 Resolution,

X2.7.2 Verification,

X2.7.3 Zeroing,

X2.7.4 Type of anvil (flat, rounded, or pointed),

X2.7.5 Cleanliness of part and anvil surfaces,

X2.7.6 User-friendliness of measuring device,

X2.7.7 Stability/temperature variations,

X2.7.8 Coating removal,

X2.7.9 Operator technique, and

X2.7.10 Ratchets or other features used to regulate the clamping force.

X2.8 Flat anvils are generally preferred for measuring the dimensions of round or flat specimens which have relatively smooth surfaces. One exception is that rounded or pointed

anvils must be used in measuring the thickness of curved specimens taken from large-diameter tubing (see Fig. 13), to prevent overstating the thickness. (Another concern for these curved specimens is the error that can be introduced through use of the equation  $A = W \times T$ ; see 7.1.3.)

X2.9 Heavy coatings should generally be removed from at least one grip end of flat specimens taken from coated products to permit accurate measurement of base metal thickness, assuming (a) the base metal properties are what are desired, (b) the coating does not contribute significantly to the strength of the product, and (c) coating removal can be easily accomplished. Otherwise, it may be advisable to leave the coating intact. Where this issue may arise, all parties involved in comparison or conformance testing should agree as to whether or not coatings are to be removed before measurement.

X2.10 As an example of how the considerations identified above affect dimensional measurement procedures, consider the case of measuring the thickness of 0.015 in. painted, flat rolled steel specimens. The paint should be removed prior to measurement, if possible. The measurement device used should have flat anvils, must read to 0.0001 in. or better, and must have excellent repeatability and reproducibility. Since GR and R is a significant concern, it will be best to use a device which has a feature for regulating the clamping force used, and devices without digital displays should be avoided to prevent reading errors. Before use of the device, and periodically during use, the anvils should be cleaned, and the device should be verified or zeroed (if an electronic display is used) or both. Finally, personnel should be trained and audited periodically to ensure that the measuring device is being used correctly and consistently by all.

## SUMMARY OF CHANGES

This section identifies the principal changes to this standard that have been incorporated since the last issue.

(1) Paragraph X2.10 was re-worded.

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